

ATS 541

Chap. 4

HW 4

$$1 = 15$$

$$2 = 10$$

$$3 = 10$$

$$4 = 5$$

$$5 = 10$$

$$50$$

(1)

$$m = 1 \text{ g.}$$

15 pts

Processer considered:

i) Heat water from $T_1 = 0$ to $T_2 = 20^\circ\text{C}$ ii) Evaporate all water ($m = 1\text{g}$) @ $T_2 = 20^\circ\text{C}$

a) ΔU : Involves both latent, sensible heating and work
 7 pt. From $dq = du + dw$ we can write

$$du = dq - p d\alpha$$

Note : dq (heating) = $m c_w dT$ (heating water) dq (evap) = $m L_{lv}$ (evap. of water)

$$W = \int p d\alpha = p \int_{\alpha_l}^{\alpha_v} d\alpha = p(\alpha_v - \alpha_l) \approx p\alpha_v$$

assume (work is involved only in the evaporation process) $[\alpha_v \gg \alpha_l]$

$$\text{Since } p\alpha_v = R_v T, \int p d\alpha \approx p\alpha_v = R_v T = W$$

Now,

$$\begin{aligned} \Delta U &= m c_w \Delta T + m L_{lv} - m R_v T \\ &= 10^{-3} \text{ kg} \left[(4218 \text{ J kg}^{-1} \text{ K}^{-1})(20 \text{ K}) + 245 \times 10^6 \text{ J kg}^{-1} \right. \\ &\quad \left. - (461 \text{ J kg}^{-1} \text{ K}^{-1})(293 \text{ K}) \right] \\ &= 2.40 \times 10^3 \text{ J} \end{aligned}$$

for 20°C

$$1 \text{ cal} = 4.184 \text{ J}$$

Assume $c_w = 4218 \text{ J kg}^{-1} \text{ K}^{-1}$ in above. (Iribarne & Gordon)
 Should use $c_w = 4190 \text{ J kg}^{-1} \text{ K}^{-1}$ (Bolton 1980)

(2)

b) Δh

4 pts

Since $dg = dh - \alpha dp$ ¹⁰ ($p = \text{const}$)

$$\Delta h = \int dh = \int dg$$

$$= m(c_w \Delta T + L_{vl}) = 10^3 \text{ kg} \left[(4218 \text{ J kg}^{-1} \text{ K}^{-1}) (20 \text{ K}) + 2.45 \times 10^6 \text{ J kg}^{-1} \right]$$

$$= 2.53 \times 10^3 \text{ J}$$

4 pts

c) Δs

$$\Delta s = \frac{dq}{T} = m c_w \int_{T_1}^{T_2} \frac{dT}{T} + \frac{m L_{vl}}{T_2}$$

$$= m \left(c_w \ln\left(\frac{T_2}{T_1}\right) + \frac{L_{vl}}{T_2} \right)$$

$$= 10^3 \text{ kg} \left[(4218 \text{ J kg}^{-1} \text{ K}^{-1}) \ln\left(\frac{293}{273}\right) + \frac{2.45 \times 10^6 \text{ J kg}^{-1}}{293 \text{ K}} \right]$$

$$= 8.67 \text{ J K}^{-1}$$

2

3

$$\Delta S_{\text{total}} = \Delta S_1 + \Delta S_2 + \Delta S_3 + \Delta S_4$$

10 pts

ΔS_1 : heat ice $T_1 = -10$ to $T_2 = 0^\circ\text{C}$

ΔS_2 : melt ice @ $T_2 = 0^\circ\text{C}$

ΔS_3 : heat water $T_2 = 0$ to $T_3 = 100^\circ\text{C}$

ΔS_4 : vaporize water @ $T_3 = 100^\circ\text{C}$.

$$\begin{aligned}\Delta S_1 &= m c_i \int_{T_0}^0 \frac{dT}{T} = (0.002 \text{ kg})(2106 \text{ J K}^{-1} \text{ kg}^{-1}) \ln \frac{273}{263} \\ &= 0.157 \text{ J K}^{-1}\end{aligned}$$

$$\begin{aligned}\Delta S_2 &= m L_{\text{ice}} / T_2 = \frac{(0.002 \text{ kg})(3.34 \times 10^5 \text{ J kg}^{-1} \text{ K}^{-1})}{273.15 \text{ K}} \\ &= 2.45 \text{ J K}^{-1}\end{aligned}$$

$$\begin{aligned}\Delta S_3 &= m c_w \int_{T_2}^{T_3} d \ln T = \frac{(0.002 \text{ kg})(4180 \text{ J kg}^{-1} \text{ K}^{-1})}{\star \ln\left(\frac{373}{273}\right)} \\ &= 2.61 \text{ J kg}^{-1}\end{aligned}$$

$$\begin{aligned}\Delta S_4 &= m L_{\text{vl}} / T_3 = \frac{(0.002 \text{ kg})(2.25 \times 10^6 \text{ J kg}^{-1} \text{ K}^{-1})}{\text{for } 100^\circ\text{C} \rightarrow 373.15 \text{ K}} \\ &= 12.06 \text{ J K}^{-1}\end{aligned}$$

$$\Delta S = \sum \Delta S_i = 17.28 \text{ J K}^{-1}$$

3. $m = 200 \text{ g}$ $p = \text{const.}$

$$\Delta S = 19.2 \text{ J K}^{-1}$$

10 pts.

$$W = 1.61 \times 10^3 \text{ J}$$

$$dq = du + \overset{(dw)}{p d\alpha} = c_p dT - \alpha dp$$

$$\Delta S = m \int \frac{dq}{T} = m c_p \int_{T_1}^{T_2} \frac{dT}{T} = m c_p \ln\left(\frac{T_2}{T_1}\right) = 19.2 \text{ J K}$$

$$\ln\left(\frac{T_2}{T_1}\right) = \frac{19.2 \text{ J K}^{-1}}{0.2 \text{ kg} \cdot 1005.7 \text{ J K}^{-1} \text{ kg}^{-1}} = .0955$$

$$\frac{T_2}{T_1} = 1.100$$

$$mW = W = m \int_{\alpha_1}^{\alpha_2} p d\alpha = m p (\alpha_2 - \alpha_1) \quad \begin{array}{l} p\alpha = RT \\ \alpha = \frac{RT}{p} \end{array}$$

$$= m p \left(\frac{RT_2}{p} - \frac{RT_1}{p} \right)$$

$$1.61 \times 10^3 \text{ J} = m R (T_2 - T_1)$$

$$T_2 - T_1 = \frac{1.61 \times 10^3 \text{ J}}{m R_d} = \frac{1.61 \times 10^3 \text{ J}}{0.2 \text{ kg} \cdot 287.05 \text{ J K}^{-1} \text{ kg}^{-1}}$$

$$= 28.04 \text{ K}$$

Then $T_2 = 1.1 T_1$

and $(1.1 T_1 - T_1) = 0.1 T_1 = 28.04 \text{ K}$

$$T_1 = 280.4$$

$$\therefore T_2 = T_1 + 28.04 = 308.44 \text{ K}$$

5 pts

5

4. Entropy conserved $\Rightarrow ds = 0 = \frac{dq}{T}$

This implies adiabatic; for which

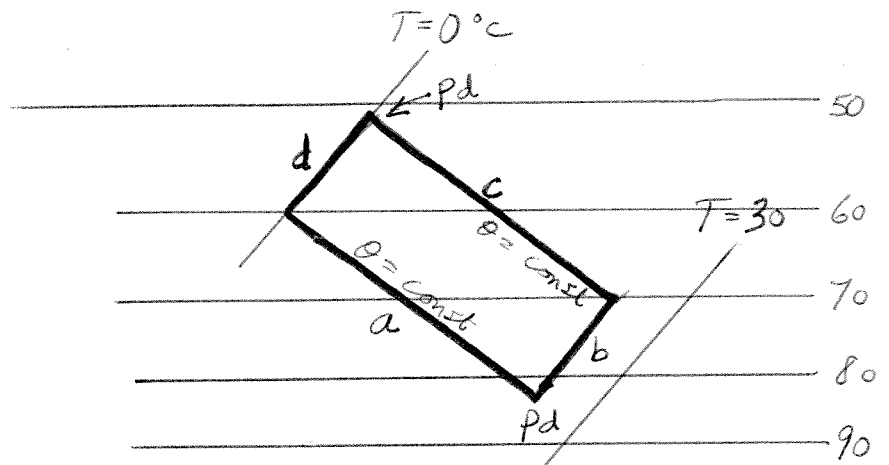
$$dq = 0 = du + dw$$

Since $dw > 0$ for an adiabatic expansion,

$du < 0$, so internal energy decreases.

5
marks
(ppts)

This Carnot cycle is traced out on the skew-T.



Section of a skew-T diagram

Two types of work involved

a) Work for an isothermal expansion ($T = \text{const}$)

$$dw = p dx$$

$$p\alpha = RT, \alpha = \frac{RT}{p}$$

$$\boxed{dw = -RT d \ln p} \quad (1)$$

$$d\alpha = -\frac{RT}{p^2} dp \quad (T = \text{const})$$

b) Work for an adiabatic change ($dq = 0$)

$$\boxed{p dx = -c_v dT} \quad (2)$$

From (2), we see that work contributed by the adiabatic expansion/compression cancels since the temp. range is the same, but inverted.

$$W_a = -c_v \int_0^{25} dT; \quad W_c = -c_v \int_{25}^0 dT$$

$$W_a + W_c = 0$$

The total work is the difference between the isothermal processes $b \rightarrow a$ and $d \rightarrow c$.

$$W_b + W_d = -RT_b \int_{p_b}^{p_a} d \ln p - RT_d \int_{p_d}^{p_c} d \ln p$$

• (next page)

5 (cont.)

We can determine p_b and p_d using

$$\frac{T}{T_0} = \left(\frac{p}{p_0}\right)^{\gamma} \quad \text{or} \quad \frac{p}{p_0} = \left(\frac{T}{T_0}\right)^{1/\gamma}$$

$$p = p_0 \left(\frac{T}{T_0}\right)^{1/\gamma}$$

$$\text{So } p_b = 60 \left(\frac{298}{273}\right)^{1/\gamma} = 81.53 \text{ kPa}$$

$$p_d = 70 \left(\frac{273}{298}\right)^{1/\gamma} = 51.51 \text{ kPa}$$

$$\therefore w_{TOT} = w_b + w_d$$

$$= -RT_b \int_{81.53}^{70} d \ln p - RT_d \int_{51.51}^{60} d \ln p$$

$$= -R \left[(298 \text{ K}) \ln\left(\frac{70}{81.53}\right) + (273 \text{ K}) \ln\left(\frac{60}{51.51}\right) \right]$$

$$= (-287 \text{ J kg}^{-1} \text{ K}^{-1}) (-45.44 + 41.65) \text{ K}$$

$$= 1087.4 \text{ J kg}^{-1}$$